Lecture 42

Determining Internal Node Values

As seen in the previous section, a finite element solution of a boundary value problem boils down to finding the best values of the constants $\{C_j\}_{j=1}^n$, which are the values of the solution at the nodes. The interior nodes values are determined by *variational principles*. Variational principles usually amount to **minimizing internal energy**. It is a physical principle that systems seek to be in a state of minimal energy and this principle is used to find the internal node values.

Variational Principles

For the differential equations that describe many physical systems, the internal energy of the system is an integral. For instance, for the steady state heat equation

$$u_{xx}(x,y) + u_{yy}(x,y) = g(x,y) \tag{42.1}$$

the internal energy is the integral

$$I[u] = \iint_R u_x^2(x,y) + u_y^2(x,y) + 2g(x,y)u(x,y)\,dA, \tag{42.2}$$

where R is the region on which we are working. It can be shown that $u(x,u)$ is a solution of (42.1) if and only if it is minimizer of $I[u]$ in (42.2).

The finite element solution

Recall that a finite element solution is a linear combination of finite element functions:

$$U(x,y) = \sum_{j=1}^{n} C_j \Phi_j(x,y),$$

where n is the number of nodes. To obtain the values at the internal nodes, we will plug $U(x,y)$ into the energy integral and minimize. That is, we find the minimum of

$$I[U]$$

for all choices of $\{C_j\}_{j=1}^m$, where m is the number of internal nodes. In this as with any other minimization problem, the way to find a possible minimum is to differentiate the quantity with respect to the variables and set the results to zero. In this case the free variables are $\{C_j\}_{j=1}^m$. Thus to find the minimizer we should try to solve

$$\frac{\partial I[U]}{\partial C_j} = 0 \qquad \text{for} \quad 1 \le j \le m. \tag{42.3}$$

We call this set of equations the **internal node equations**. At this point we should ask whether the internal node equations can be solved, and if so, is the solution actually a minimizer (and not a maximizer). The following two facts answer these questions. These facts make the finite element method practical:

- For most applications the internal node equations are linear.
- For most applications the internal node equations give a minimizer.

We can demonstrate the first fact using an example.

Application to the steady state heat equation

If we plug the candidate finite element solution $U(x,y)$ into the energy integral for the heat equation (42.2), we obtain

$$I[U] = \iint_R U_x(x,y)^2 + U_y(x,y)^2 + 2g(x,y)U(x,y)\,dA. \tag{42.4}$$

Differentiating with respect to C_j we obtain the internal node equations

$$0 = \iint_R 2U_x \frac{\partial U_x}{\partial C_j} + 2U_y \frac{\partial U_y}{\partial C_j} + 2g(x,y)\frac{\partial U}{\partial C_j}\,dA \quad \text{for} \quad 1 \le j \le m. \tag{42.5}$$

Now we have several simplifications. First note that since

$$U(x,y) = \sum_{j=1}^{n} C_j \Phi_j(x,y),$$

we have

$$\frac{\partial U}{\partial C_j} = \Phi_j(x,y)\,.$$

Also note that

$$U_x(x,y) = \sum_{j=1}^{n} C_j \frac{\partial}{\partial x}\Phi_j(x,y),$$

and so

$$\frac{\partial U_x}{\partial C_j} = (\Phi_j)_x.$$

Similarly, $\frac{\partial U_y}{\partial C_j} = (\Phi_j)_y$. The integral (42.5) then becomes

$$0 = 2\iint U_x(\Phi_j)_x + U_y(\Phi_j)_y + g(x,y)\Phi_j(x,y)\,dA \quad \text{for} \quad 1 \le j \le m.$$

Next we use the fact that the region R is subdivided into triangles $\{T_i\}_{i=1}^{p}$ and the functions in question have different definitions on each triangle. The integral then is a sum of the integrals:

$$0 = 2\sum_{i=1}^{p} \iint_{T_i} U_x(\Phi_j)_x + U_y(\Phi_j)_y + g(x,y)\Phi_j(x,y)\,dA \quad \text{for} \quad 1 \le j \le m.$$

Now note that the function $\Phi_j(x,y)$ is linear on triangle T_i and so

$$\Phi_{ij}(x,y) = \Phi_j|_{T_i}(x,y) = a_{ij} + b_{ij}x + c_{ij}y.$$

This gives us the simplifications

$$(\Phi_{ij})_x(x,y) = b_{ij} \quad \text{and} \quad (\Phi_{ij})_y(x,y) = c_{ij}.$$

Also, U_x and U_y restricted to T_i have the form

$$U_x = \sum_{k=1}^{n} C_k b_{ik} \quad \text{and} \quad U_y = \sum_{k=1}^{n} C_k c_{ik}.$$

The internal node equations then reduce to

$$0 = \sum_{i=1}^{p} \iint_{T_i} \left(\sum_{k=1}^{n} C_k b_{ik} \right) b_{ij} + \left(\sum_{k=1}^{n} C_k c_{ik} \right) c_{ij} + g(x,y)\Phi_{ij}(x,y)\, dA \quad \text{for} \quad 1 \le j \le m.$$

Now notice that $\left(\sum_{k=1}^{n} C_k b_{ik}\right) b_{ij}$ is just a constant on T_i, and, thus, we have

$$\iint_{T_i} \left(\sum_{k=1}^{n} C_k b_{ik} \right) b_{ij} + \left(\sum_{k=1}^{n} C_k c_{ik} \right) c_{ij} = \left[\left(\sum_{k=1}^{n} C_k b_{ik} \right) b_{ij} + \left(\sum_{k=1}^{n} C_k c_{ik} \right) c_{ij} \right] A_i,$$

where A_i is just the area of T_i. Finally, we apply the Three Corners rule to make an approximation to the integral

$$\iint_{T_i} g(x,y)\Phi_{ij}(x,y)\, dA\,.$$

Since $\Phi_{ij}(x_k,y_k) = 0$ if $k \neq j$ and even $\Phi_{ij}(x_j,y_j) = 0$ if T_i does not have a corner at (x_j,y_j), we get the approximation

$$\Phi_{ij}(x_j,y_j)g(x_j,y_j)A_i/3.$$

If T_i does have a corner at (x_j,y_j) then $\Phi_{ij}(x_j,y_j) = 1$.

Summarizing, the internal node equations are

$$0 = \sum_{i=1}^{p} \left[\left(\sum_{k=1}^{n} C_k b_{ik} \right) b_{ij} + \left(\sum_{k=1}^{n} C_k c_{ik} \right) c_{ij} + \frac{1}{3} g(x_j,y_j)\Phi_{ij}(x_j,y_j) \right] A_i \quad \text{for} \quad 1 \le j \le m.$$

While not pretty, these equations are in fact linear in the unknowns $\{C_j\}$.

Experiment

Download the program `myfiniteelem.m`. This program produces a finite element solution for the steady state heat equation without source term:

$$u_{xx} + u_{yy} = 0\,.$$

To use it, you first need to set up the region and boundary values by running a script such as `mywasher.m` or `mywedge.m`. Try different settings for the boundary values `z`. You will see that the program works no matter what you choose.

Exercises

42.1 For this exercise, use the region that you made in Exercise 41.1.

- Set non-constant boundary values and plot.
- Then run `myfiniteelem.m` and plot.

Does the second plot look like it satisfies a variational principle? Why or why not? Turn in the two plots and your answers to the questions.

Review of Part IV

Methods and Formulas

Initial Value Problems

Reduction to First order system:

For an n-th order equation that can be solved for the n-th derivative

$$x^{(n)} = f\left(t, x, \dot{x}, \ddot{x}, \ldots, \frac{d^{n-1}x}{dt^{n-1}}\right) \tag{42.6}$$

use the standard change of variables:

$$\begin{aligned} y_1 &= x \\ y_2 &= \dot{x} \\ &\vdots \\ y_n &= x^{(n-1)} = \frac{d^{n-1}x}{dt^{n-1}}. \end{aligned} \tag{42.7}$$

Differentiating results in a first-order system:

$$\begin{aligned} \dot{y}_1 &= \dot{x} = y_2 \\ \dot{y}_2 &= \ddot{x} = y_3 \\ &\vdots \\ \dot{y}_n &= x^{(n)} = f(t, y_1, y_2, \ldots, y_n). \end{aligned} \tag{42.8}$$

Euler's method:

$$\mathbf{y}_{i+1} = \mathbf{y}_i + hf(t_i, \mathbf{y}_i).$$

Modified (or Improved) Euler method:

$$\begin{aligned} \mathbf{k}_1 &= hf(t_i, \mathbf{y}_i) \\ \mathbf{k}_2 &= hf(t_i + h, \mathbf{y}_i + \mathbf{k}_1) \\ \mathbf{y}_{i+1} &= \mathbf{y}_i + \frac{1}{2}(\mathbf{k}_1 + \mathbf{k}_2) \end{aligned}$$

Boundary Value Probems

Finite Differences:

Replace the Differential Equation by Difference Equations on a grid.
Review the lecture on Numerical Differentiation.

Explicit Method Finite Differences for Parabolic PDE (heat):

$$u_t \mapsto \frac{u_{i,j+1} - u_{ij}}{k} \quad \text{and} \quad u_{xx} \mapsto \frac{u_{i-1,j} - 2u_{ij} + u_{i+1,j}}{h^2} \tag{42.9}$$

leads to

$$u_{i,j+1} = ru_{i-1,j} + (1-2r)u_{i,j} + ru_{i+1,j},$$

where $h = L/m$, $k = T/n$, and $r = ck/h^2$. The stability condition is $r < 1/2$.

Implicit Method Finite Differences for Parabolic PDE (heat):

$$u_t \mapsto \frac{u_{i,j+1} - u_{ij}}{k} \quad \text{and} \quad u_{xx} \mapsto \frac{u_{i+1,j+1} - 2u_{i,j+1} + u_{i-1,j+1}}{h^2} \tag{42.10}$$

leads to

$$u_{i,j} = -ru_{i-1,j+1} + (1+2r)u_{i,j+1} - ru_{i+1,j+1},$$

which is always stable and has truncation error $O(h^2 + k)$.

Crank-Nicholson Method Finite Differences for Parabolic PDE (heat):

$$-ru_{i-1,j+1} + 2(1+r)u_{i,j+1} - ru_{i+1,j+1} = ru_{i-1,j} + 2(1-r)u_{i,j} + ru_{i+1,j},$$

which is always stable and has truncation error $O(h^2 + k^2)$.

Finite Difference Method for Elliptic PDEs:

$$u_{xx} + u_{yy} = f(x,y) \mapsto \frac{u_{i+1,j} - 2u_{ij} + u_{i-1,j}}{h^2} + \frac{u_{i,j+1} - 2u_{ij} + u_{i,j-1}}{k^2} = f(x_i, y_j) = f_{ij},$$

Finite Elements:

Based on triangles instead of rectangles.
Can be used for irregularly shaped objects.
An element: Pyramid shaped function at a node.
A finite element solution is a linear combination of finite element functions:

$$U(x,y) = \sum_{j=1}^{n} C_j \Phi_j(x,y),$$

where n is the number of nodes, and where U is an approximation of the true solution.
C_j is the value of the solution at node j.
C_j at the boundary nodes are given by boundary conditions.
C_j at interior nodes are determined by variation principles.
The last step in determining C_j's is solving a linear system of equations.

Matlab

Initial value problem solver that uses the Runge-Kutta 45 method, which has error $O(h^5)$. The input $y0$ is the initial vector and `tspan` is the time span. You can either make f a vector valued anonymous function and do

```
≫ df = @(t,y)[-y(2);y(1)]
≫ [T Y ] = ode45(dy,tspan,y0)
```

or make a function program that outputs a vector

```
function dy = myf(t,y)
    dy = [-y(2);y(1)];
end
```

and then do

```
≫ [T Y ] = ode45(@myf,tspan,y0)
```

The program `ode45` and other Matlab IVP solvers use adaptive step size to achieve a desired local and global accuracy, with a default of `tol` $= 10^{-6}$ for the global error.

The chief benefit of higher order methods and variable step size is that they allow a program to take only as few steps as necessary.